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DECIMETER BAND RADIOMETER AND MEASUREMENT OF JUPITER'S PROPER EMISSION

by

O. N. Rzhiga,
G. I. Slobodenyuk,
V. N. Titov,
Z. G. Trunova

[USSR]

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DECIMETER BAND RADIOMETER AND MEASUREMENT OF JUPITER'S PROPER EMISSION

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G. I. Slobodenyuk,
V. N. Titov,
Z. G. Trunova

SUMMARY

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This paper deals with the observations of Jupiter's proper emission intensity in the frequency of about 700 Mc/s in October 1963. The modulation radiometer, used to that effect, is described.

The results of these observations corroborate the law of Jupiter's proper emission intensity variation with wavelength, corresponding to measurements by other observers in shorter and longer wavelengths.

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We conducted in October 1963 the measurement of Jupiter's proper emission intensity in the frequency of ~ 700 mc/sec., using for measurements a modulation radiometer, of which the block-diagram is is presented in Fig. 1.

The radiometer's antenna system consists of two identical antennas (A₁, A₂), oriented in the same direction. Both antenna feeders are connected by means of a double T- branch (TB) [1], whose outputs are alternately switched to receiver (R) with the help of a transfer switch (TS). Follow at receiver output behind the quadratic detector, a modulation frequency amplifier (MFA), a synchronous detector (SD) with an integrating circuit, a d.c. amplifier and a registering device (RD).

At double T-branch output, the oscillations of both antennas are compounded in phase at point a, and in counterphase at point b.

^{*} RADIOMETR DETSIMETROVOGO DIAPAZONA I IZMERENIYE SOBSTVENNOGO IZLUCHE-NIYA YUPITERA.

The variation of current at radiometer output during passage of a point source with constant velocity through the radiation pattern in the plane of antennas $^{1}A_{1}$ and A_{2} electrical axes, repeats in its form the difference between the "overall" and "differential" radiation patterns of the antenna system, taken at outputs of the double T-branch respectively at points \underline{a} and \underline{b} .

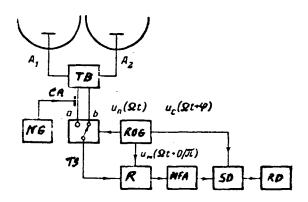
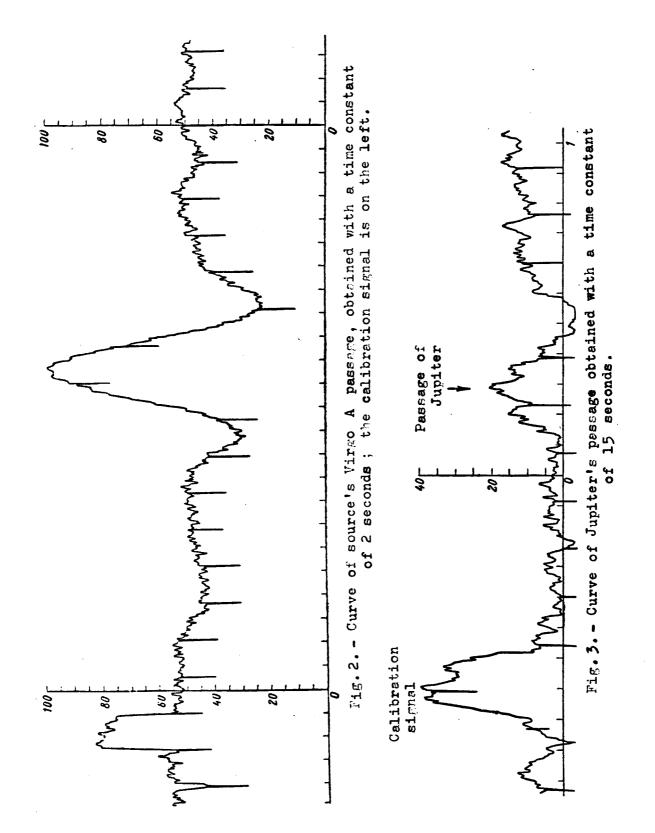


Fig. 1. - Block-diagram of the radiometer:

A₁, A₂ - antennas; TB - double T-branch; TS - antenna transfer switch; R - superheterodyne receiver with quadratic detector; MFA - modulation frequency amplifier; SD - synchr. detector; RD - registering device; ROG - rectangular oscillation generator; NG - noise generator; CA - capacitance attenuator.

A coaxial line transfer switch was worked out on parametric semiconductor diodes for alternate switching of receiver to points $\underline{\mathbf{a}}$ and $\underline{\mathbf{b}}$ of the double \mathbf{T} - branch [2].

The incomplete identity of electrical characteristics of the double T- branch's channels may induce a parasitic signal impairing the sensitivity of the radiometer. In order to eliminate the parasitic signal on the grid of one of amplifier tubes of intermediate frequency, a modulated voltage um of rectangular form, fed from the generator ROG (Fig. 1), whose polarity either coincides or is opposite to um voltage, arrives to transfer switch. Prior to measurements, the polarity and the amplitude of modulating voltage are so chosen, that the variation of MFA's amplification factor, caused by periodical shift of the operating point of tube's characteristic, smooth off the signal level difference at detector output in both positions of the transfer switch TS.



The modulation frequency is chosen sufficiently high — 525 cps so as to exclude the effects of fluctuations of receiving circuit amplification, and not multiple of 50 cps, so as to rid ourselves of interferences from the harmonics of the feeding grid. The MFA has a pass-band of 10 cps.

The synchronous detector (SD) is assembled according to a ring circuit on semiconductor silica diodes AlOlA. The time constant of the integrating RC-filter at its output was chosen equal to 1, 2, 5, 10 or 15 seconds.

The rectangular oscillation generator (ROG) consists of quartz-stabilized generator to a frequency of 1050 cps, from which short pulses setting on a trigger cell, are formed by means of limitation and differentiation. At trigger output there is obtained a rectangular oscillation with recurrence frequency F = 525 cps. This rectangular oscillation is fed to the transfer switch u_{π} for the IFA modulation (intermediate frequency amplifier modulation) — u_{M} and to the synchronous detector u_{c} . The oscillation, fed to the synchronous detector, is preliminarly shifted in phase by an angle φ for the compensation of signal lag in the narrow-band circuit of the MFA.

A noise generator (NG) is utilized for the calibration of the radiometer.

The fluctuation sensitivity of the radiometer with a 15 sec time constant of the integrating circuit constituted 0.40 K.

When observing the sources the radiometer antenna was set with a $1-2^{\circ}$ advance by azimuth. Tracking was conducted only by the angle of the spot. The passage of the discrete source Virgo A (M-87) through the antenna system's radiation pattern is plotted in Fig. 2. A standard noise signal, serving for the calibration of the radiometer, is shown on registrations. Minute annotations seen on registrations, were given for tying the time. A typical curve of single Jupiter passage is plotted in Fig. 3.

The determination of the intensity of received emission from Jupiter was conducted by the standard noise signal, calibrated with the

aid of the source Virgo A. The density of this source's emission flux in the frequency of 960 mc/s constitutes $300 \cdot 10^{-26} \,\mathrm{wm^{-2}\,cps^{-1}}$, while the spectral index is -0.72 [3]. Using these data we computed the density of this source's emission flux for the frequency, at which measurements were conducted.

For the computation of the equivalent temperature of Jupiter we applied the expression

$$T_{\rm H} = \frac{S_{\rm H} \lambda_0^3 P_{\rm EO}}{2k\Omega_{\rm EO} P_{\rm H}} , \qquad (1)$$

where $S_{\rm M}$ is the density of the radio emission of Virgo A in the wavelength $\lambda_{\rm O}$; $P_{\rm M}$ and $P_{\rm M}$ are respectively the powers of Jupiter and Virgo A emissions in the band Δf , reduced to receiver input; the ratio $P_{\rm M}/P_{\rm m}$ is determined from observations; k is the Boltzmann constant; $Q_{\rm M}$ is the solid angle of the planet.

The expression (1) was obtained with the help of the following correlations:

$$P_{\rm m} = \frac{1}{2} S_{\rm m} A_{\rm eff} \Delta f = \frac{S_{\rm m} \lambda_0^2 \Delta f}{2\Omega_{\rm m}}, \qquad (2)$$

$$P_{10} = kT_{\rm H}\Delta f \frac{\Omega_{10}}{\Omega_{2}} , \qquad (3)$$

where $A_{\frac{1}{2}}$ is the effective area of the antenna; Δf is the radiometer band to the detector; Q_a is the solid angle of the ray of antenna system's radiation pattern.

The value of the mean Jupiter's equivalent temperature, obtained from a series of observations, constituted 12 000°K (upon conversion to visible dimensions of the planet) with a root-mean-square error of 2000°K. In this value of the error the inaccurate knowledge of the orientation of antenna's polarization ellipses and Jupiter emission and the lack of precision in the determination of Virgo A flux density (4%) is taken into account [4].

The results of observations, expounded in the given paper, corroborate the law of Jupiter emission intensity variation with wavelength (see Fig. 4, next page), corresponding to measurements by other observers

in shorter or longer wavelengths, refer to [5 - 12].

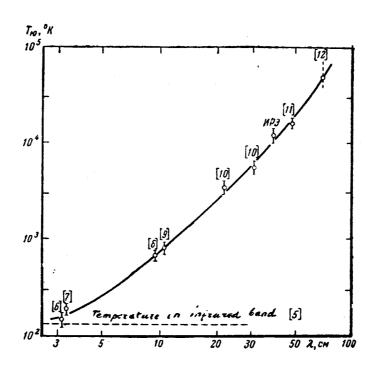


Fig. 4. - Variation of the mean equivalent temperature of Jupiter with wavelength according to observations by various authors, including those of the present paper.

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**** THE END ****

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